

Unit - 1

Basics

of

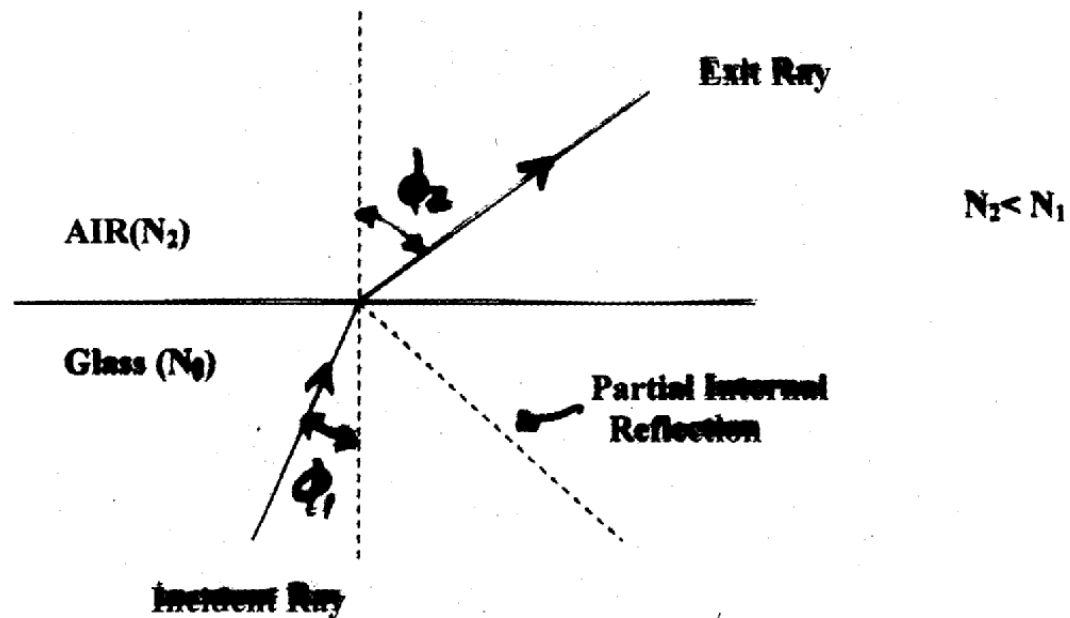
Transmission of Light

## RAY THEORY TRANSMISSION

**REF INDEX**

$$n = \frac{\text{VELOCITY OF LIGHT IN VACCUM}}{\text{VELOCITY OF LIGHT IN THE MEDIUM}}$$

- THE DENSER THE MEDIUM, THE LOWER IS THE VELOCITY OF LIGHT



SNELL'S LAW  $N_1 \sin \phi_1 = N_2 \sin \phi_2$

CRITICAL ANGLE( $\phi_c$ ) ANGLE OF INCIDENCE FOR WHICH ANGLE OF REFRACTION IS  $90^\circ$

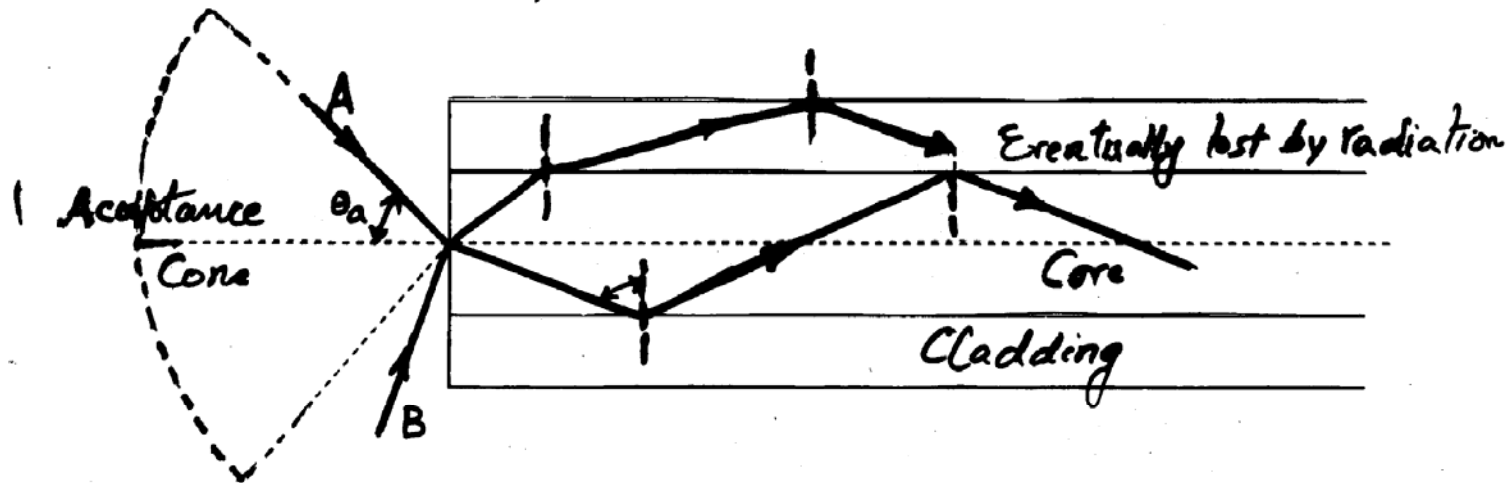
$$N_1 \sin \phi_c = N_2$$

$$N_1/N_2 = 1/\sin \phi_c \text{ OR } \sin \phi_c = N_2/N_1$$

AT ANGLE OF INCIDENCE, GREATER THAN  $\phi_c$ , THE LIGHT IS REFLECTED BACK INTO THE ORIGINATING DIELECTRIC MEDIUM ( $\eta = 99.9\%$ )

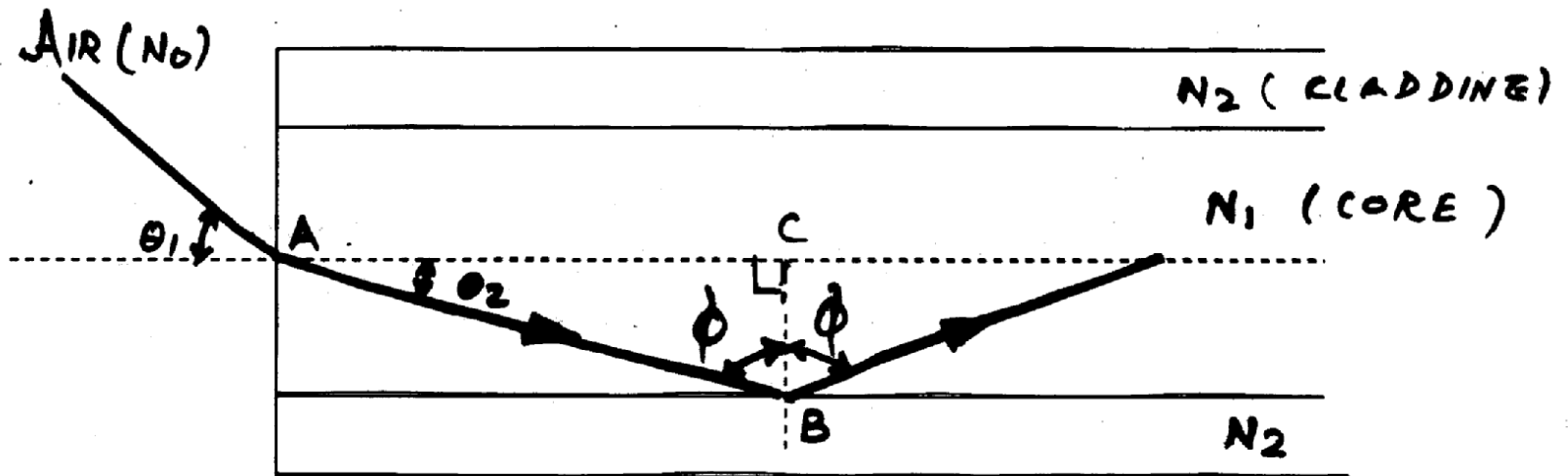
→ TOTAL INTERNAL REFLECTION .

ACCEPTANCE ANGLE ( $\theta_a$ ) - LIGHT LAUNCHED INTO AN OPT. FIBER



- NOT ALL RAYS ENTERING THE FIBER CORE WILL CONTINUE TO BE PROPAGATED DOWN ITS LENGTH.
- RAYS TO BE TRANSMITTED BY TIR WITHIN THE FIBER CORE MUST BE INCIDENT ON THE FIBER CORE WITHIN THE ACCEPTANCE CONE (HALF ANGLE =  $\phi_a$ )
- $\phi_a$  = MAXIMUM ACCEPTANCE ANGLE FOR THE FIBER.

## NUMERICAL APERTURE (NA)

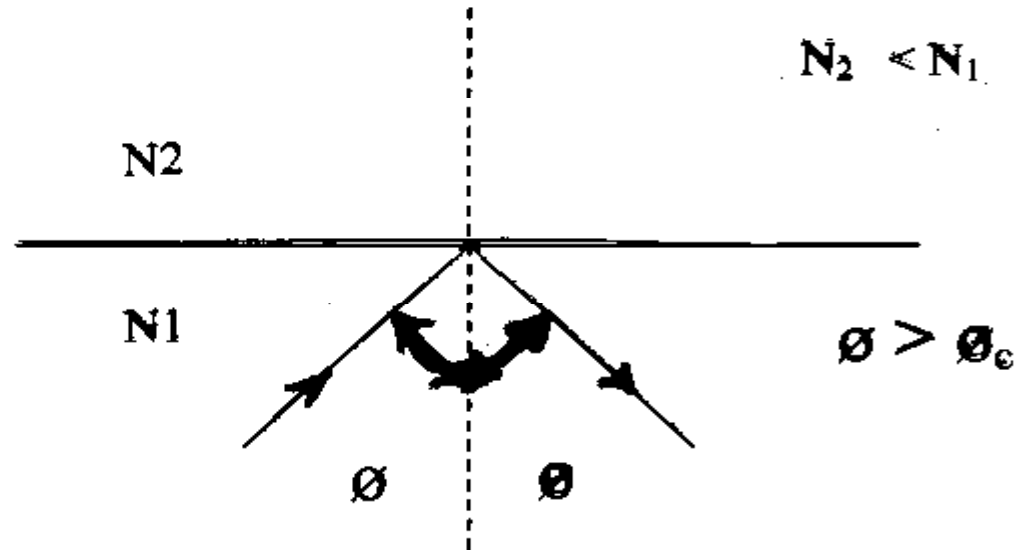


THREE MEDIA- CORE/ CLADDING/ AIR

$\theta_1 < \theta_a$  (ACCEPTANCE ANGLE)

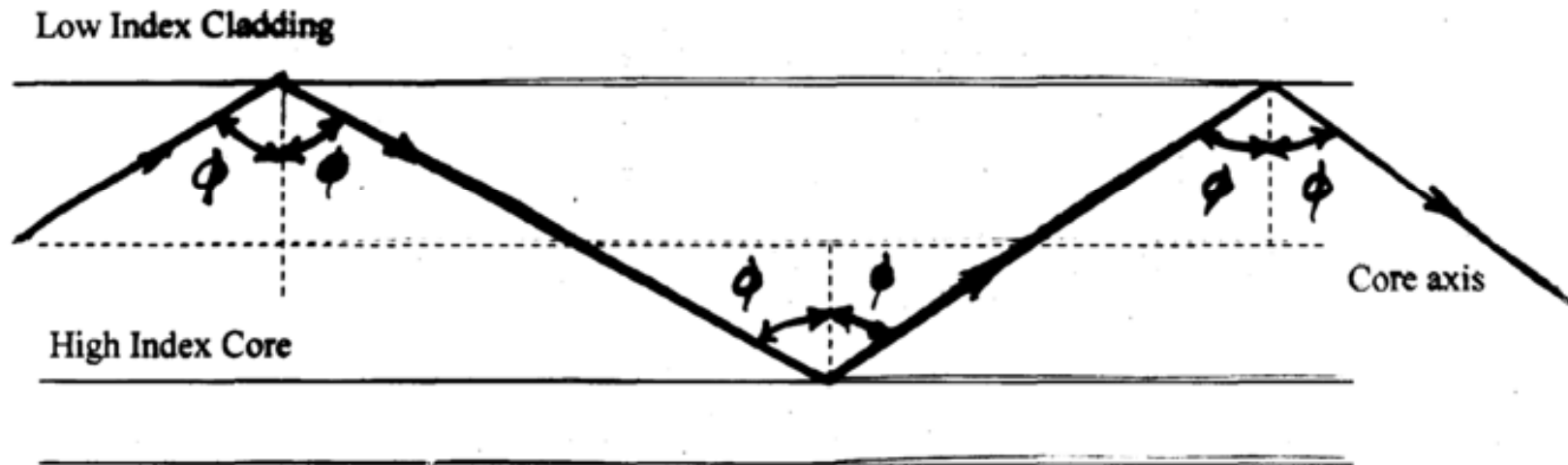
$N_2 < N_1$

## TOTAL INTERNAL REFLECTION (TIR)



- TIR OCCURS WHEN ANGLE OF INCIDENCE EXCEEDS THE CRITICAL ANGLE.

- LIGHT TRAVELS DOWN AN OPTICAL FIBER AT A SHALLOW ANGLE (LESS THAN  $90^\circ - \theta_c$ ) VIA A SERIES OF TOTAL INTERNAL REFLECTIONS



## TRANSMISSION OF LIGHT RAY IN A PERFECT OPTICAL FIBER

IMPERFECTIONS AT THE CORE CLADDING INTERFACE WOULD RESULT IN LOSSES OF THE LIGHT RAY INTO THE CLADDING

$$N_0 \sin \theta_1 = N_1 \sin \theta_2 \text{-----1}$$

$$\text{IN } \Delta ABC \phi = \pi/2 - \theta_2 \text{ OR } \theta_2 = (\pi/2 - \phi)$$

WHERE  $\phi > \phi_c$

$$\text{EQUATION (1) BECOMES } N_0 \sin \theta_1 = N_1 \sin \theta_2 = N_1 \sin (\pi/2 - \phi)$$

$$\text{i.e. } N_0 \sin \theta_1 = N_1 \cos \phi$$

$$\text{USING } \sin^2 \phi + \cos^2 \phi = 1$$

$$N_0 \sin \theta_1 = N_1 (1 - \sin^2 \phi)^{1/2}$$

### **LIMITING CASE FOR TIR**

$$\phi = \phi_c, \theta_1 = \theta_a, \sin \phi_c = N_2/N_1$$

$$N_0 \sin \theta_a = N_1 (1 - N_2^2/N_1^2)^{1/2} = (N_1^2 - N_2^2)^{1/2}$$

$$NA = N_0 \sin \theta_a = (N_1^2 - N_2^2)^{1/2} = \sin \theta_a$$



(SINCE  $N_0 = 1$  FOR AIR)

THE OPTICAL RAY WILL BE PROPAGATED ALONG  
THE FIBER FOR  $0 \leq \theta_1 \leq \theta_a$

NA IS INDEPENDENT OF THE FIBER CORE DIA

LET  $\Delta = \frac{N_1^2 - N_2^2}{2N_1^2}$  = RELATIVE REF. INDEX DIFF.  
BETWEEN CORE & CLADDING.

HENCE  $NA = N_1 (2 \Delta)^{1/2}$